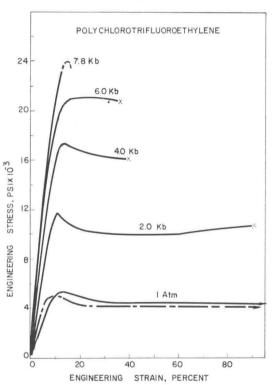
The low-temperature nominal stress–strain curves for polycarbonate are presented in fig. 5. Again there was a general increase of modulus, yield stress and strain, and a decrease of fracture strain, which was quite drastically reduced in the small region between  $273^{\circ} \text{K}$  and  $253^{\circ} \text{K}$ , unlike the high-pressure results.





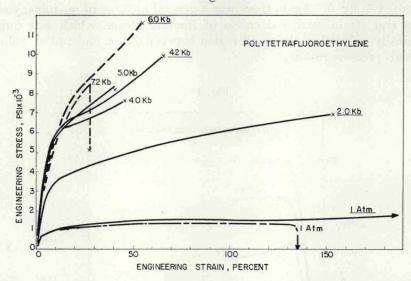
Engineering tensile stress–strain curves for polychlorotrifluorethylene at various pressures.

## 3.2.1. Yield criteria

Applied mathematical formulations using relevant parameters have been constructed to predict the failure in any definable stress state. These rely on the condition that when a particular parameter reaches some 'critical' value by application of a system of stresses, the specimen will fail. For yielding, the most useful parameters are the maximum and octahedral shear stresses,  $\tau_{\rm max}$  and  $\tau_{\rm oct}\dagger$ , respectively. If the critical value of this

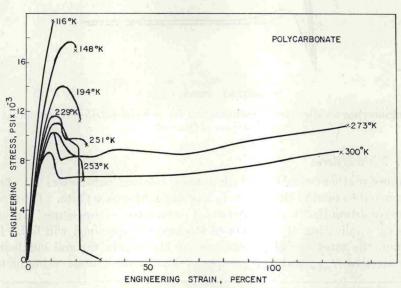
<sup>†</sup> The magnitude of the maximum shear stress  $\tau_{\rm max}$  is calculated as  $(\sigma_1 - \sigma_3)/2$ , where  $\sigma_1$  and  $\sigma_3$  are the algebraically largest and smallest principal normal streses, respectively. The octahedral shear stress is equal to  $[(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2]^{1/2}/3$ .

Fig. 4



Engineering tensile stress–strain curves for polytetrafluorethylene at various pressures.

Fig. 5



Engineering tensile stress–strain curves for polycarbonate at various temperatures.